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M.E. CHEMICAL 1ST YEAR

DATE:20.01.22

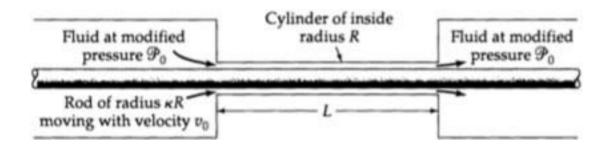
SUBJECT: TRANSPORT PHENOMENA

TIME: 60 MIN

Q1. A cylindrical rod of diameter κR moves axially with velocity v_0 along the axis of a cylindrical cavity of radius R. The pressure at both ends of the cavity is the same, so that the fluid moves through the annular region solely because of the rod motion.

(a) Find the velocity distribution the annular region. in narrow (b) Find the mass rate of flow through the annular region. (c) Obtain the viscous force acting on the rod over the length L.

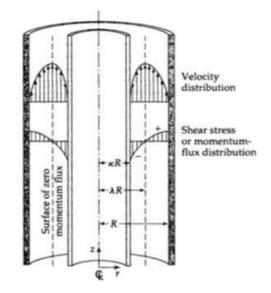
Solve by using equation of change. (CO3) (4,2,2)



Q2. (a) Heat is flowing through an annular wall of inside radius r_0 and outside radius r_1 . The thermal conductivity varies linearly with temperature from k_0 at T_0 to k_1 at T_1 . Develop an expression for the heat flow through the wall.

(b) Show how the expression in (a) can be simplified when $(r_1 - r_0)/r_0$ is very small.(CO1)(4,3)

Q3. (a) Consider steady-state axial flow of an incompressible liquid in an annular region between two coaxial cylinders of radii κR and R. The fluid is flowing upward in the tube—that is, in the direction opposed to gravity. Determine the momentum-flux and velocity distributions, maximum and average velocity, mass rate of flow and force exerted by the fluid on the solid surfaces.



(b) A horizontal annulus, 27 ft in length, has an inner radius of 0.495 in. and an outer radius of 1.1 in. A 60% aqueous solution of sucrose is to be pumped through the annulus at 20°C. At this temperature the solution density is 80.3 lb/ft³ and the viscosity is 136.8 lb_m/ft.hr. What is the volume flow rate when the impressed pressure difference is 5.39 psi? (CO2) (5,5)

§B.6 EQUATION OF MOTION FOR A NEWTONIAN FLUID WITH CONSTANT ρ AND μ

$[\rho D \mathbf{v} / D t = -\nabla p + \mu \nabla^2 \mathbf{v} + \rho \mathbf{g}]$		
Cartesian coordinates (x, y, z):		
$\rho\left(\frac{\partial v_s}{\partial t} + v_s \frac{\partial v_s}{\partial x} + v_s \frac{\partial v_s}{\partial y} + v_s \frac{\partial v_s}{\partial z}\right) = -\frac{\partial p}{\partial x} + \mu\left[\frac{\partial^2 v_s}{\partial x^2} + \frac{\partial^2 v_s}{\partial y^2} + \frac{\partial^2 v_s}{\partial z^2}\right] + \rho g_s$	(8.6-1)	
$\rho\left(\frac{\partial v_s}{\partial t} + v_s \frac{\partial v_s}{\partial x} + v_y \frac{\partial v_s}{\partial y} + v_s \frac{\partial v_s}{\partial z}\right) = -\frac{\partial p}{\partial y} + \mu\left[\frac{\partial^2 v_s}{\partial x^2} + \frac{\partial^2 v_y}{\partial y^2} + \frac{\partial^2 v_y}{\partial z^2}\right] + \rho g_y$	(8.6-2)	
$\rho\left(\frac{\partial v_s}{\partial t} + v_s \frac{\partial v_s}{\partial x} + v_p \frac{\partial v_s}{\partial y} + v_s \frac{\partial v_s}{\partial z}\right) = -\frac{\partial p}{\partial z} + \mu\left[\frac{\partial^3 v_s}{\partial x^2} + \frac{\partial^3 v_s}{\partial y^2} + \frac{\partial^3 v_s}{\partial z^2}\right] + \rho g_s$	(8.6-3)	

 $\frac{Cylindrical \ coordinates}{\rho\left(\frac{\partial v_{t}}{\partial t} + v_{t}\frac{\partial v_{t}}{\partial \tau} + \frac{v_{s}}{r}\frac{\partial v_{s}}{\partial \theta} + v_{t}\frac{\partial v_{s}}{\partial z} - \frac{v_{s}^{2}}{r}\right) = -\frac{\partial p}{\partial \tau} + \mu\left[\frac{\partial}{\partial r}\left(\frac{1}{r}\frac{\partial}{\partial \tau}(rv_{t})\right) + \frac{1}{r^{2}}\frac{\partial^{2}v_{s}}{\partial \theta^{2}} + \frac{\partial^{2}v_{s}}{\partial z^{2}} - \frac{2}{r^{2}}\frac{\partial v_{s}}{\partial \theta}\right] + \rho g, \quad (B.6-4)$ $\rho\left(\frac{\partial v_{s}}{\partial t} + v_{s}\frac{\partial v_{s}}{\partial \tau} + \frac{v_{s}}{r}\frac{\partial v_{s}}{\partial \theta} + v_{s}\frac{\partial v_{s}}{\partial z} + \frac{v_{s}v_{s}}{r}\right) = -\frac{1}{r}\frac{\partial p}{\partial \theta} + \mu\left[\frac{\partial}{\partial \tau}\left(\frac{1}{r}\frac{\partial}{\partial r}(rv_{s})\right) + \frac{1}{r^{2}}\frac{\partial^{2}v_{s}}{\partial \theta^{2}} + \frac{\partial^{2}v_{s}}{\partial z^{2}} + \frac{2}{r^{2}}\frac{\partial v_{s}}{\partial \theta}\right] + \rho g, \quad (B.6-5)$ $\rho\left(\frac{\partial v_{s}}{\partial t} + v_{s}\frac{\partial v_{s}}{\partial \tau} + \frac{v_{s}}{r}\frac{\partial v_{s}}{\partial \theta} + v_{s}\frac{\partial v_{s}}{\partial z}\right) = -\frac{\partial p}{\partial z} + \mu\left[\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial v_{s}}{\partial r}\right) + \frac{1}{r^{2}}\frac{\partial^{2}v_{s}}{\partial \theta^{2}} + \frac{\partial^{2}v_{s}}{\partial z^{2}}\right] + \rho g, \quad (B.6-6)$

Spherical coordinates (r, 0, 6):	1
$\rho\left(\frac{\partial v_{s}}{\partial t} + v_{r}\frac{\partial v_{s}}{\partial r} + \frac{v_{s}}{r}\frac{\partial v_{s}}{\partial \theta} + \frac{v_{s}}{r}\frac{\partial v_{s}}{\sin \theta}\frac{\partial v_{s}}{\partial \phi} - \frac{v_{s}^{2} + v_{s}^{2}}{r}\right) = -\frac{\partial p}{\partial r}$	
$+ \mu \left[\frac{1}{r^2} \frac{\partial^2}{\partial r^2} (r^2 v_i) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial v_i}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 v_i}{\partial \phi^2} \right] + \rho g_i$	(8.6-77
$\rho\left(\frac{\partial v_{\mu}}{\partial t} + v_{r}\frac{\partial v_{\mu}}{\partial r} + \frac{v_{\mu}}{r}\frac{\partial v_{\mu}}{\partial \theta} + \frac{v_{\mu}}{r}\frac{\partial v_{\mu}}{\sin\theta}\frac{\partial v_{\mu}}{\partial \phi} + \frac{v_{r}v_{\mu} - v_{\mu}^{2}\cot\theta}{r}\right) = -\frac{1}{r}\frac{\partial p}{\partial \theta}$	
$+\mu\left[\frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2\frac{\partial v_\theta}{\partial r}\right)+\frac{1}{r^2}\frac{\partial}{\partial \theta}\left(\frac{1}{\sin\theta}\frac{\partial}{\partial \theta}(v_\theta\sin\theta)\right)+\frac{1}{r^2}\frac{\partial}{\sin^2\theta}\frac{\partial^2 v_\theta}{\partial \phi^2}+\frac{2}{r^2}\frac{\partial v_r}{\partial \theta}-\frac{2\cot\theta}{r^2}\frac{\partial v_\theta}{\partial \phi}\right]+\rho g_\theta$	(8.6-8)
$\rho\left(\frac{\partial v_{\theta}}{\partial t} + v_{r}\frac{\partial v_{\theta}}{\partial r} + \frac{v_{\theta}}{r}\frac{\partial v_{\theta}}{\partial \theta} + \frac{v_{\theta}}{r\sin\theta}\frac{\partial v_{\theta}}{\partial \phi} + \frac{v_{\theta}v_{r} + v_{\theta}v_{\theta}\cot\theta}{r}\right) = -\frac{1}{r\sin\theta}\frac{\partial p}{\partial \phi}$	
$+ \mu \left[\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial v_\theta}{\partial r} \right) + \frac{1}{r^2} \frac{\partial}{\partial \theta} \left(\frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \left(v_\theta \sin \theta \right) \right) + \frac{1}{r^2} \frac{\partial^2 v_\theta}{\sin^2 \theta} \frac{\partial^2 v_\theta}{\partial \phi^2} + \frac{2}{r^2} \frac{\partial v_\theta}{\sin \theta} \frac{\partial^2 v_\theta}{\partial \phi} + \frac{2}{r^2} \frac{\cot \theta}{\sin \theta} \frac{\partial v_\theta}{\partial \phi} \right] + \rho g$	(8.6-9)

* The quantity in the brackets in Eq. B.6-7 is not what one would expect from Eq. (b0 for $[\nabla \cdot \nabla v]$ in Table A.7-3, because we have added to Eq. (b0 the expression for $(2/r)(\nabla \cdot v)$, which is zero for fluids with constant p. This gives a much simpler equation.

§B.5 THE EQUATION OF MOTION IN TERMS OF τ

 $[\rho D \mathbf{v} / D t = -\nabla p - [\nabla \cdot \tau] + \rho \mathbf{g}]$

Cartesian coordinates (x, y, z):*					
	$\rho\left(\frac{\partial v_s}{\partial t} + v_s \frac{\partial v_s}{\partial x} + v_y \frac{\partial v_s}{\partial y} + v_s \frac{\partial v_s}{\partial z}\right) = -\frac{\partial p}{\partial z} - \left[\frac{\partial}{\partial x}\tau_{ss} + \frac{\partial}{\partial y}\tau_{ys} + \frac{\partial}{\partial z}\tau_{ss}\right]$	+ pg.	(8.5-1)		
	$\rho\left(\frac{\partial v_y}{\partial t} + v_x \frac{\partial v_y}{\partial x} + v_y \frac{\partial v_y}{\partial y} + v_x \frac{\partial v_y}{\partial z}\right) = -\frac{\partial p}{\partial y} - \left[\frac{\partial}{\partial x}\tau_{xy} + \frac{\partial}{\partial y}\tau_{yy} + \frac{\partial}{\partial z}\tau_{xy}\right]$	+ pg,	(8.5-2)		
	$\rho\left(\frac{\partial v_i}{\partial t} + v_i \frac{\partial v_i}{\partial x} + v_j \frac{\partial v_i}{\partial y} + v_i \frac{\partial v_i}{\partial z}\right) = -\frac{\partial p}{\partial z} - \left[\frac{\partial}{\partial x}\tau_{i1} + \frac{\partial}{\partial y}\tau_{j1} + \frac{\partial}{\partial z}\tau_{i2}\right]$	+ PSI	(8.5-3)		

⁴ These equations have been written without making the assumption that τ is symmetric. This means, for example, that when the usual assumption is made that the stress tensor is symmetric, τ_{ij} and τ_{ji} may be interchanged.

Cylindrical coordinates (r, 0, z). ^b		
$\rho\left(\frac{\partial v_i}{\partial t} + v_i\frac{\partial v_i}{\partial r} + \frac{v_i}{r}\frac{\partial v_i}{\partial \theta} + v_i\frac{\partial v_i}{\partial z} - \frac{v_i^2}{r}\right) = -\frac{\partial p}{\partial r} - \left[\frac{1}{r}\frac{\partial}{\partial r}\left(r\tau_{ir}\right) + \frac{1}{r}\frac{\partial}{\partial \theta}\tau_{ir} + \frac{\partial}{\partial z}\tau_{ir} - \frac{\tau_{ir}}{r}\right] + \rho g,$	(8.5-4)	
$p\left(\frac{\partial v_{\theta}}{\partial t} + v_{t}\frac{\partial v_{\theta}}{\partial r} + \frac{v_{\theta}}{r}\frac{\partial v_{\theta}}{\partial \theta} + v_{t}\frac{\partial v_{\theta}}{\partial z} + \frac{v_{t}v_{\theta}}{r}\right) = -\frac{1}{r}\frac{\partial p}{\partial \theta} - \left[\frac{1}{r^{2}}\frac{\partial}{\partial r}(r^{2}\tau_{\theta}) + \frac{1}{r}\frac{\partial}{\partial \theta}\tau_{\theta\theta} + \frac{\partial}{\partial z}\tau_{\theta\theta} + \frac{\tau_{\theta} - \tau_{\theta}}{r}\right] + pg_{\theta}$	(8.5-5)	
$\rho\left(\frac{\partial v_{i}}{\partial t} + v_{i}\frac{\partial v_{i}}{\partial r} + \frac{v_{i}}{r}\frac{\partial v_{i}}{\partial \theta} + v_{i}\frac{\partial v_{i}}{\partial z}\right) = -\frac{\partial p}{\partial z} - \left[\frac{1}{r}\frac{\partial}{\partial r}(r\tau_{u}) + \frac{1}{r}\frac{\partial}{\partial \theta}\tau_{u} + \frac{\partial}{\partial z}\tau_{u}\right] + \rho g_{u}$	(8.5-6)	

⁹ These equations have been written without making the assumption that v is symmetric. This means, for example, that when the usual assumption is made that the stress tensor is symmetric, $\tau_w - \tau_w \approx 0$.

Spherical coordinates (r, 0, 4)."	
$p\left(\frac{\partial v_{r}}{\partial t} + v_{r}, \frac{\partial v_{r}}{\partial r} + \frac{v_{s}}{r}\frac{\partial v_{r}}{\partial \theta} + \frac{v_{4}}{r}\frac{\partial v_{r}}{\sin\theta}\frac{\partial v_{r}}{\partial \phi} - \frac{v_{4}^{2} + v_{4}^{2}}{r}\right) = -\frac{\partial p}{\partial r}$	(14) (14) (14) (14) (14) (14) (14) (14)
$-\left[\frac{1}{r^2}\frac{\partial}{\partial r}(r^2r_w)+\frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(r_w\sin\theta)+\frac{1}{r\sin\theta}\frac{\partial}{\partial \phi}r_w-\frac{r_w+r_{ee}}{r}\right]+\rho g,$	(8.5-7)
$p\left(\frac{\partial v_{\mu}}{\partial t} + v_{\mu}\frac{\partial v_{\mu}}{\partial r} + \frac{v_{\mu}}{r}\frac{\partial v_{\mu}}{\partial \theta} + \frac{v_{\mu}}{r}\frac{\partial v_{\mu}}{\sin \theta}\frac{\partial v_{\mu}}{\partial \phi} + \frac{v_{\nu}v_{\mu} - v_{\mu}^2 \cot \theta}{r}\right) = -\frac{1}{r}\frac{\partial p}{\partial \theta}$	
$+\left[\frac{1}{r^{2}}\frac{\partial}{\partial r}(r^{2}r_{ss})+\frac{1}{r\sin\theta}\frac{\partial}{\partial \theta}(r_{ss}\sin\theta)+\frac{1}{r\sin\theta}\frac{\partial}{\partial \phi}r_{ss}+\frac{(r_{ss}-r_{ss})-r_{ss}\cot\theta}{r}\right)+\rho g_{s},$	(8.5-8)
$\rho\left(\frac{\partial v_a}{\partial t} + v_r, \frac{\partial v_a}{\partial r} + \frac{v_a}{r} \frac{\partial v_a}{\partial \theta} + \frac{v_a}{r} \frac{\partial v_a}{\sin \theta} \frac{\partial v_a}{\partial \phi} + \frac{v_a v_r + v_b v_a}{r} \frac{\cot \theta}{r}\right) = -\frac{1}{r} \frac{\partial p}{\sin \theta} \frac{\partial p}{\partial \phi}$	
$-\left[\frac{1}{r^{2}}\frac{\partial}{\partial r}(r^{2}\tau_{r\phi})+\frac{1}{r\sin\theta}\frac{\partial}{\partial\theta}(\tau_{s\phi}\sin\theta)+\frac{1}{r\sin\theta}\frac{\partial}{\partial\phi}\tau_{s\phi}+\frac{(\tau_{\phi}-\tau_{r\phi})+\tau_{e\theta}\cot\theta}{r}\right]+\rho_{e\theta}^{*}$	(8.5-9)

⁶ These equations have been written without making the assumption that τ is symmetric. This means, for example, that when the usual assumption is made that the stress tensor is symmetric, $\tau_{ac} = \tau_{ac} = 0$.